

SIFAT VOLUMETRIK FLUIDA MURNI

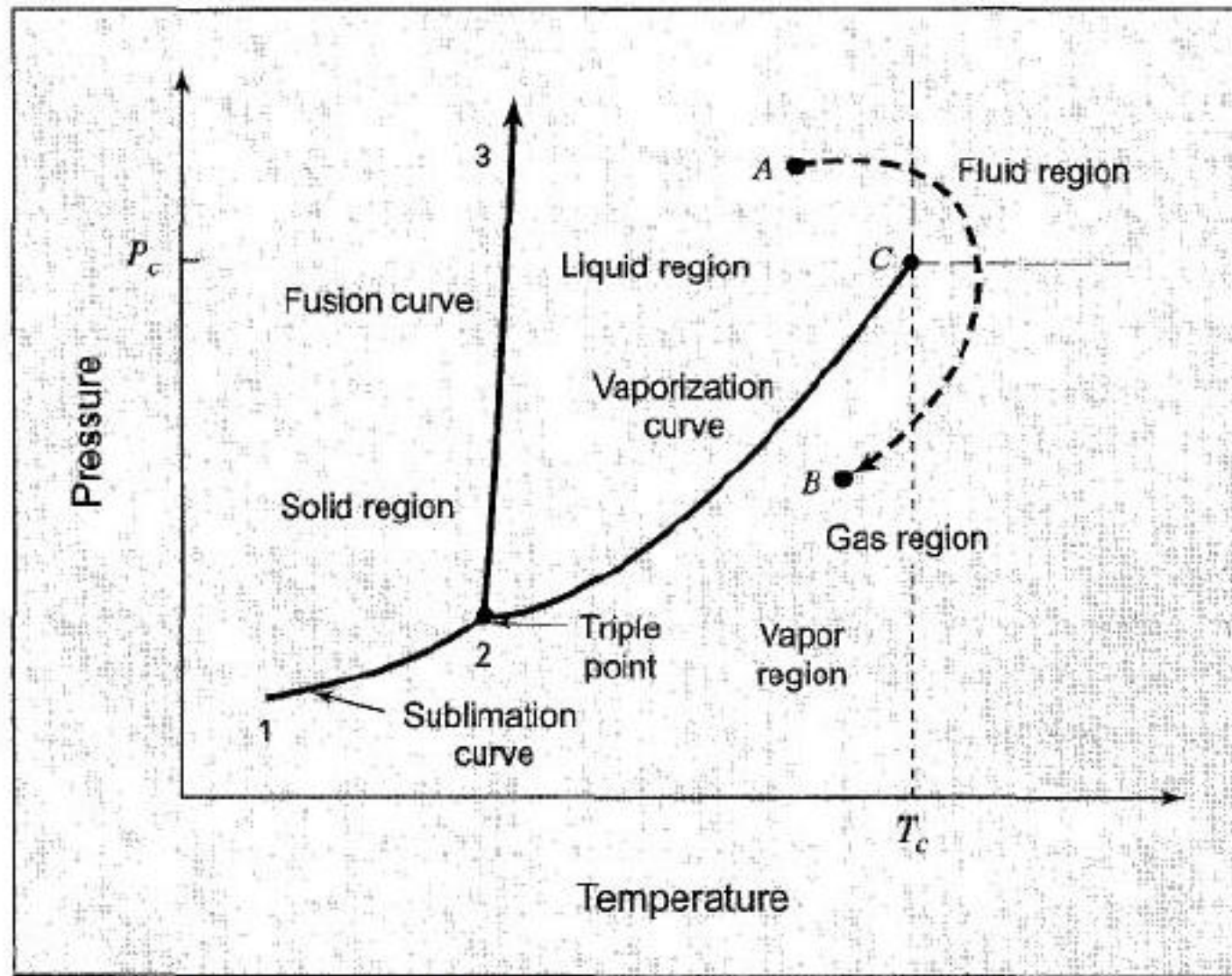


Figure 3.1 P T diagram for a pure substance

Kaidah Fase Gibbs

Pada Kesetimbangan Fase dan tidak ada reaksi kimia, berlaku :

$$F = 2 - \pi + N$$

Dengan :

F = derajat kebebasan

π = jumlah fase

N = jumlah komponen

$$F = 2 - \pi + N$$

Contoh:

Air (cair) setimbang dengan uapnya

$$F = 2 - 2 + 1 = 1$$

Pada kurva penguapan :

$$\pi = 2, N = 1 \rightarrow F = 2 - 2 + 1 = 1$$

Jadi pd kurva penguapan kita bisa memilih T tertentu, atau P tertentu. Tapi ingat hanya 1 pilihan T saja atau P saja, yg lain mengikuti saja.

Derajat kebebasan pada titik tripel:

$$\pi = 3, N = 1 \rightarrow F = 2 - 3 + 1 = 0$$

Jadi Titik Tripel sudah tertentu.

Persamaan Keadaan (Equation of State = EOS)

adalah :

Persamaan yang menunjukkan hubungan antara P, V dan T suatu zat

atau

$$f(P, V, T) = 0$$

Khas untuk tiap zat

Gas Ideal

- ✓ EOS berbentuk : $PV = RT$
atau $Z = PV/RT$ dan $Z = 1$

dengan

Z = faktor kompresibilitas

P = pressure, Pa

V = volume molar, m^3/mol

T = temperature absolut, K

R = konstanta gas umum,

$$= 8,314 \text{ m}^3 \text{ Pa mol}^{-1} \text{ K}^{-1} = 8,314 \text{ J mol}^{-1} \text{ K}^{-1}$$

Untuk satuan lain, lihat appendix A SVNA

- ✓ $U = f(T)$ Energi dalam hanya fungsi suhu
- ✓ Berlaku pada tekanan sangat rendah

Contoh :

Hitung densitas gas Nitrogen (g/cm^3) pada tekanan 1 atm dan suhu 30°C ? (Asumsi: Gas ideal)

Jawab: ??

Hubungan antar Sifat pada Gas Ideal

$$C_v = \left(\frac{\partial U}{\partial T} \right)_v = \frac{dU}{dT} = C_v(T)$$

$$H = U + PV = U(T) + RT = H(T)$$

$$C_p = \left(\frac{\partial H}{\partial T} \right)_p = \frac{dH}{dT} = C_p(T)$$

$$C_p = \frac{dH}{dT} = \frac{dU}{dT} + \frac{d(RT)}{dT} = C_v + R \rightarrow \boxed{C_p = C_v + R}$$

$$dU = C_v dT \qquad \Delta U = \int C_v dT$$

$$dH = C_p dT \qquad \Delta H = \int C_p dT$$

Perhitungan Proses dengan Persamaan Gas Ideal

PROSES ?

Proses-proses yg akan dibahas (untuk sistem tertutup), a.l. :

1. Proses Isotermal
2. Proses Isobarik
3. Proses Isokhorik
4. Proses Adiabatik

Proses Isotermal ($\Delta T = 0$)

$$\Delta U = C_v \Delta T = 0 \quad \text{ingat} \quad \left(\frac{\partial U}{\partial T} \right)_v = C_v$$

$$\Delta H = C_p \Delta T = 0 \quad \text{ingat} \quad \left(\frac{\partial H}{\partial T} \right)_p = C_p$$

$$\Delta U = Q + W = 0$$

$$Q = -W = \int_{V_1}^{V_2} P \, dV \quad (\text{ingat } P = \frac{RT}{V})$$

$$Q = -W = \int_{V_1}^{V_2} \frac{RT}{V} \, dV = RT \ln \frac{V_2}{V_1}$$

$$(\text{ingat } \frac{P_1 V_1}{T_1} = \frac{P_2 V_2}{T_2} \text{ dan } T_2 = T_1 \text{ sehingga } \frac{V_2}{V_1} = \frac{P_1}{P_2})$$

$$Q = -W = RT \ln \frac{P_1}{P_2} = -RT \ln \frac{P_2}{P_1} = RT \ln \frac{V_2}{V_1} \quad (\text{T tetap})$$

Proses Isobarik

$$\Delta U = \int C_v dT \quad \text{dan} \quad \Delta H = \int C_p dT$$

$$Q = \Delta H = \int C_p dT \quad (P \text{ tetap})$$

$$\begin{aligned} W &= -\int P dV = -P \int dV = -\int R dT = -R \int dT \\ &= -R (T_2 - T_1) = -P (V_2 - V_1) \end{aligned}$$

Cek dgn Hk I : $\Delta U = Q + W$

$$C_v dT = C_p dT - R dT$$

$$C_v = C_p - R \rightarrow C_p = C_v + R$$

Proses Isokhorik ($\Delta V=0$)

$$\Delta U = \int C_v dT \quad \text{dan} \quad \Delta H = \int C_p dT$$

$$Q = \Delta U = \int C_v dT \quad (V \text{ tetap})$$

$=0$

$$W = -\int P dV = 0 \rightarrow W = 0$$

$$\text{Cek dgn Hk I : } \Delta U = Q + W \rightarrow \Delta U = Q$$

Proses Adiabatik ($Q=0$)

The diagram shows the derivation of adiabatic equations. It starts with a box containing $dQ + dW = C_V dT$, where dQ is crossed out with a red diagonal line and a red arrow points to it. An arrow points from this box to the right, leading to the equation $\frac{T_2}{T_1} = \left(\frac{P_2}{P_1}\right)^{R/C_P}$. Another arrow points down from the first box to a second box containing $\frac{dT}{T} = -\frac{R}{C_V} \frac{dV}{V}$. From this second box, an arrow points to the right, leading to the equation $\frac{T_2}{T_1} = \left(\frac{V_2}{V_1}\right)^{R/C_V}$. To the right of these two equations, a bracket groups them and points to a box containing $PV^\gamma = \text{tetap}$. Below this box is another box containing $\gamma \equiv \frac{C_P}{C_V}$.

$$\cancel{dQ} + dW = C_V dT$$
$$\frac{T_2}{T_1} = \left(\frac{P_2}{P_1}\right)^{R/C_P}$$
$$dW = -PdV$$
$$\frac{dT}{T} = -\frac{R}{C_V} \frac{dV}{V}$$
$$\frac{T_2}{T_1} = \left(\frac{V_2}{V_1}\right)^{R/C_V}$$
$$PV^\gamma = \text{tetap}$$
$$\gamma \equiv \frac{C_P}{C_V}$$

$$TV^{\gamma-1} = \text{tetap} \rightarrow T_1 V_1^{\gamma-1} = T_2 V_2^{\gamma-1}$$
$$T P^{(1-\gamma)/\gamma} = \text{tetap}$$
$$P V^\gamma = \text{tetap}$$

$\gamma = 1,67$ pada gas monoatomik (He, Ne, Ar dsb)

$\gamma = 1,4$ pada gas diatomik (H_2 , N_2 , O_2)

$\gamma = 1,3$ pada gas poli atomik sederhana (CO_2 , SO_2 , NH_3 , CH_4)

Proses Adiabatik (lanjutan)

dari Hk I: $\Delta U = Q + W \rightarrow W = \Delta U$

$$W = \int C_v dT = C_v \Delta T \quad (C_v = \frac{R}{\gamma - 1})$$

$$= \frac{R}{\gamma - 1} \Delta T = \frac{RT_2 - RT_1}{\gamma - 1} = \frac{P_2 V_2 - P_1 V_1}{\gamma - 1}$$

$$W = \frac{P_1 V_1}{\gamma - 1} \left[\left(\frac{P_2}{P_1} \right)^{\frac{\gamma - 1}{\gamma}} - 1 \right] = \frac{RT_1}{\gamma - 1} \left[\left(\frac{P_2}{P_1} \right)^{\frac{\gamma - 1}{\gamma}} - 1 \right]$$

Proses Politropik

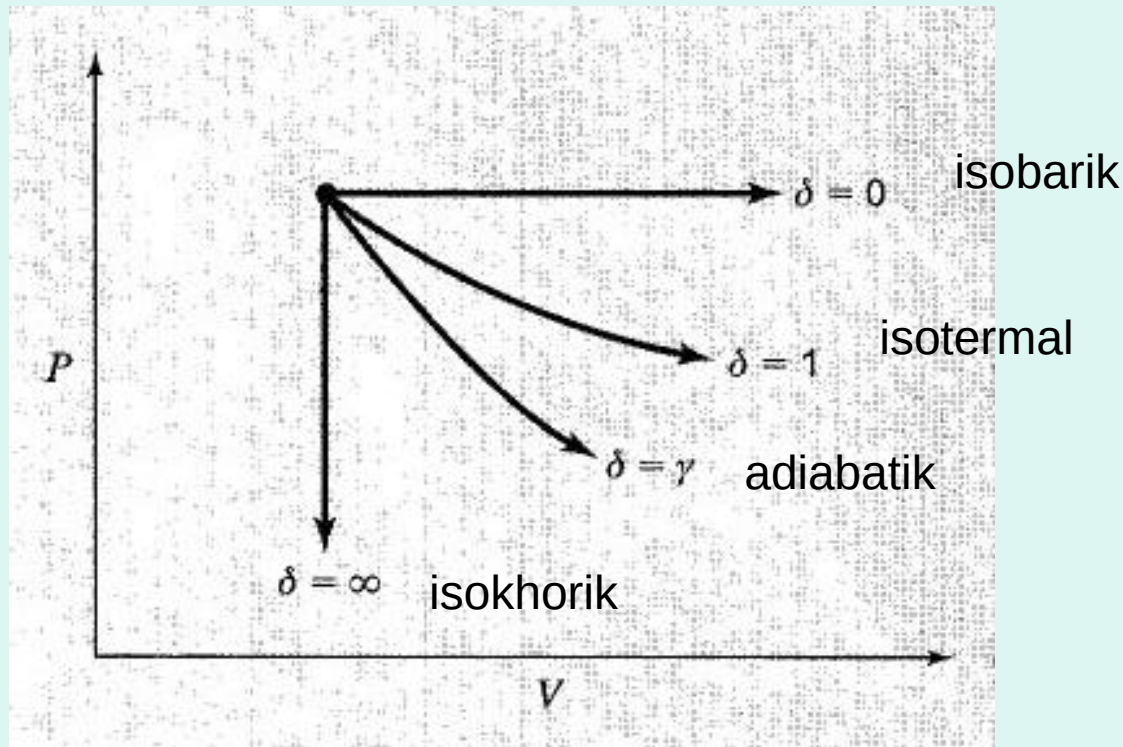
"turning many ways" $\rightarrow \delta = \text{konstan}$

$$T V^{\delta-1} = \text{tetap} \rightarrow T_1 V_1^{\delta-1} = T_2 V_2^{\delta-1}$$

$$T P^{(1-\delta)/\delta} = \text{tetap}$$

$$P V^{\delta} = \text{tetap}$$

$$W = \frac{P_1 V_1}{\delta - 1} \left[\left(\frac{P_2}{P_1} \right)^{\frac{\delta-1}{\delta}} - 1 \right] = \frac{RT_1}{\delta - 1} \left[\left(\frac{P_2}{P_1} \right)^{\frac{\delta-1}{\delta}} - 1 \right]$$



Gas Non Ideal

$$Z = PV/RT \quad Z \neq 1 \quad (Z = \text{faktor kompresibilitas})$$

EOS untuk gas non ideal:

1. Bentuk Virial

$$\text{a. } Z = 1 + B'P + C'P^2 + D'P^3 + \dots$$

$$\text{b. } Z = 1 + \frac{B}{V} + \frac{C}{V^2} + \frac{D}{V^3} + \dots$$

B' , C' , D' dst dan B , C , D dst : koefisien virial

2. Bentuk Kubik (Cubic EOS) (Pangkat Tiga)

a.l.

□ Persamaan Van der Waals :

$$P = \frac{RT}{V-b} - \frac{a}{V^2}$$

Dalam bentuk polinomial :

$$V^3 - \left(b + \frac{RT}{P} \right) V^2 + \frac{a}{P} V - \frac{ab}{P} = 0$$

$$a = \frac{27}{64} \frac{R^2 T_c^2}{P_c}$$

$$b = \frac{1}{8} \frac{RT_c}{P_c}$$

T_c = suhu kritis

P_c = tekanan kritis

❑ Persamaan Redlich-Kwong

$$P = \frac{RT}{V-b} - \frac{a}{V(V+b)\sqrt{T}}$$

$$a = 0,42748 \frac{R^2 T_c^{2,5}}{P_c}$$



$$b = 0,08664 \frac{RT_c}{P_c}$$



(Pada buku SVNA mrpk parameter ψ dan Ω)

□ Persamaan Soave-Redlich-Kwong

$$P = \frac{RT}{V - b} - \frac{a(T)}{V(V + b)}$$

$$a(T_c) = a_c = 0,42748 \frac{(RT_c)^2}{P_c}$$

$$b = 0,08664 \frac{RT_c}{P_c}$$

$$a(T) = a_c \cdot \alpha(T)$$

$$T_r = \frac{T}{T_c}$$

$$m = 0,480 + 1,574\omega - 0,176\omega^2$$

$$\alpha(T) = \left(1 + m(1 - \sqrt{T_r})\right)^2$$

ω = acentric factor (lihat tabel) → faktor bentuk molekul
seberapa dekat dengan bentuk bola

- ❑ Pers. bentuk kubik lain masih banyak lagi, tetapi cukup 3 pers. di atas sebagai contoh.
- ❑ Persamaan bentuk kubik membentuk kurva sbb:

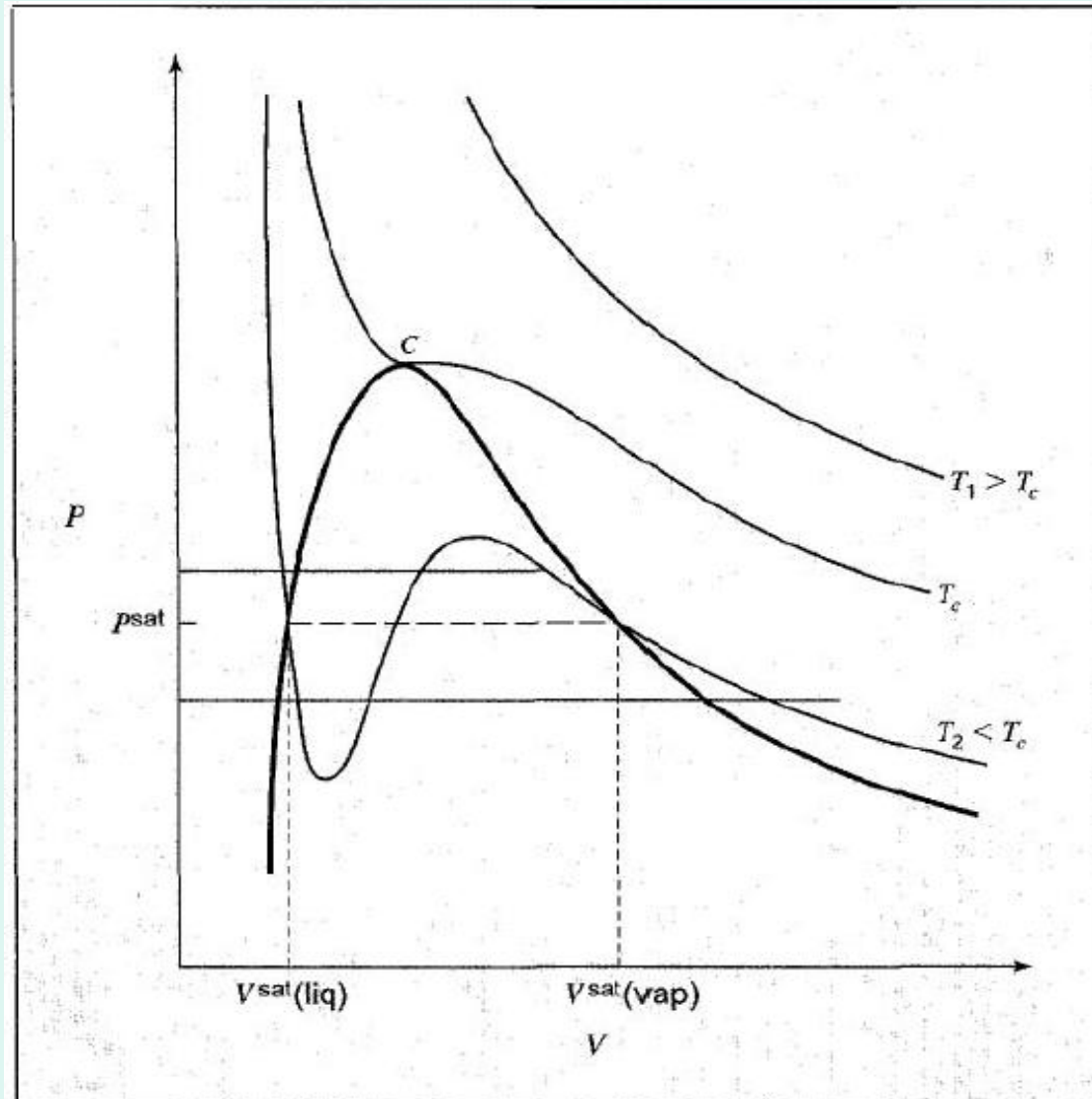


Figure 3.12 Isotherms as given by a cubic equation of state

Application of the virial equations

- Differentiation:

$$\left(\frac{\partial Z}{\partial P}\right)_T = B' + 2C'P + 3D'P^2 + \dots \quad \left(\frac{\partial Z}{\partial P}\right)_{T;P=0} = B'$$

- the virial equation truncated to two terms satisfactorily represent the PVT behavior up to about 5 bar

$$Z = 1 + B'P \quad Z = 1 + \frac{BP}{RT} = 1 + \frac{B}{V} \longrightarrow \text{At low pressure}$$

- the virial equation truncated to three terms provides good results for pressure range above 5 bar but below the critical pressure

$$Z = 1 + B'P + C'P^2 \quad Z = 1 + \frac{B}{V} + \frac{C}{V^2}$$

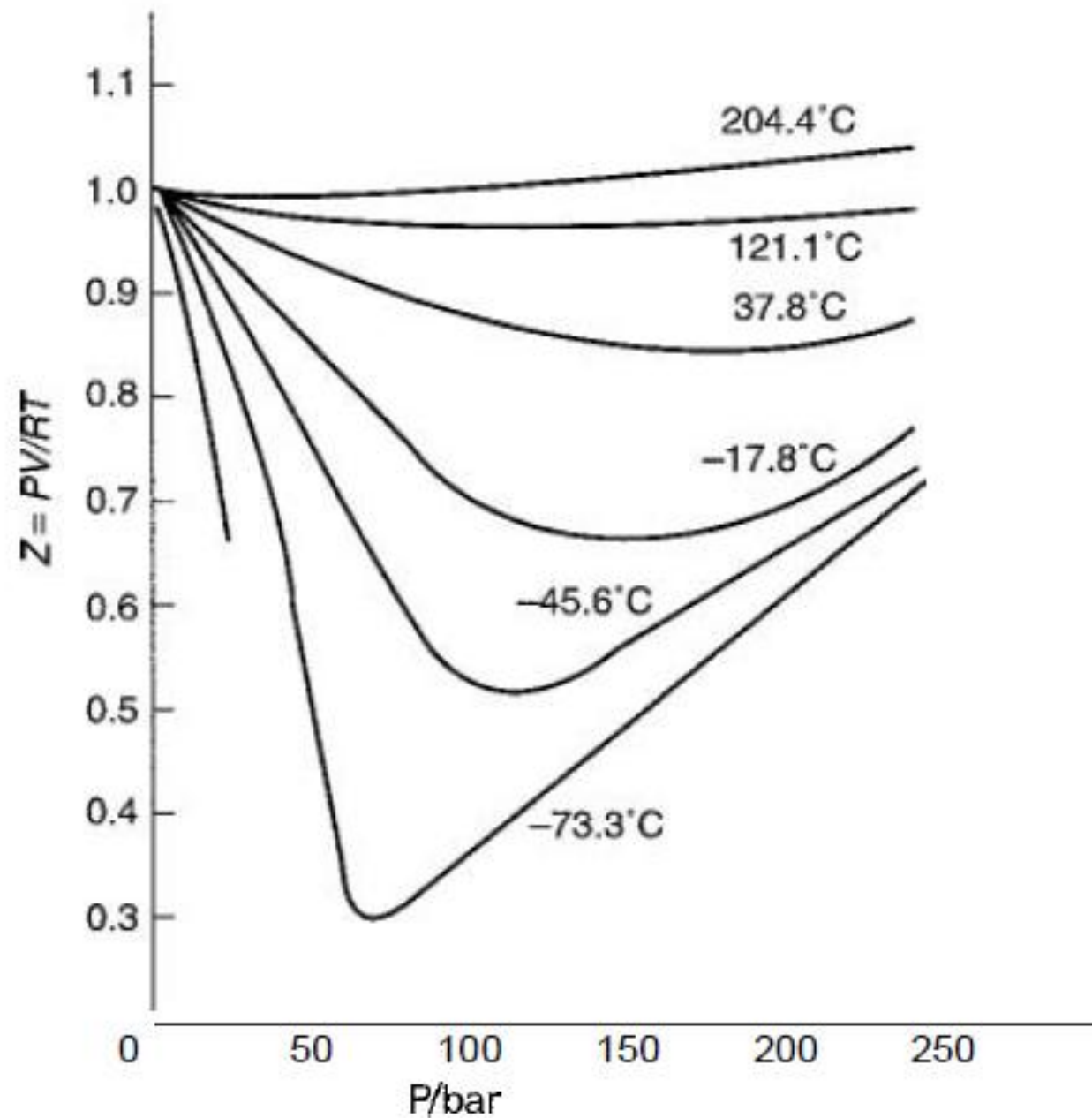


Figure 3.10 Compressibility-factor graph for methane

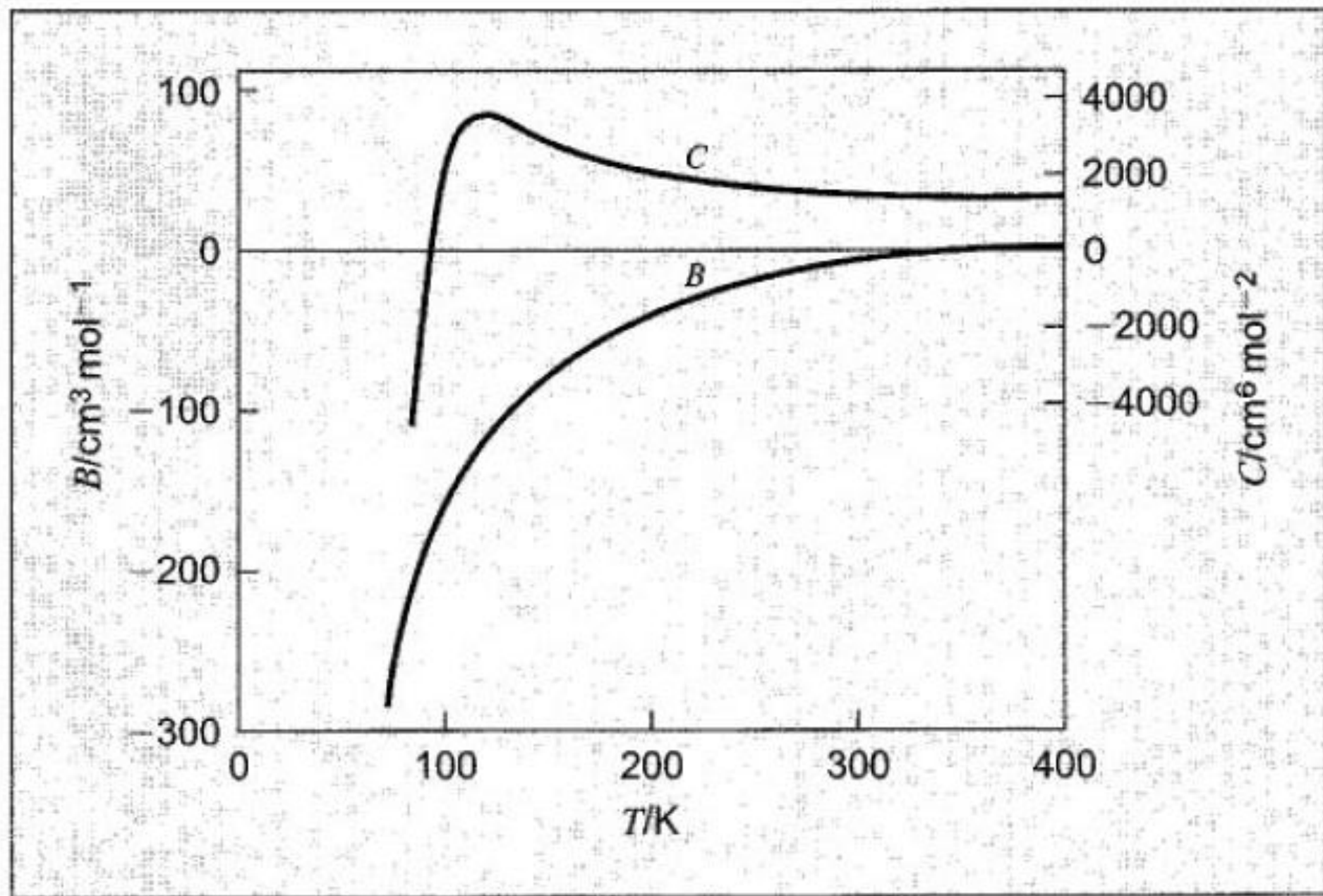


Figure 3.1 1 Density-series virial coefficients B and C for nitrogen

Reported values for the virial coefficients of isopropanol vapor at 200°C are:

$B = -388 \text{ cm}^3/\text{mol}$ and $C = -26000 \text{ cm}^6/\text{mol}^2$. Calculate V and Z for isopropanol vapor at 200 °C and 10 bar by (1) the ideal gas equation; (2) two-term virial equation; (3) three-term virial equation.

(1) For an ideal gas, $Z = 1$:

$$V = \frac{RT}{P} = \frac{83.14 \times 473.15}{10} = 3934 \text{ cm}^3/\text{mol}$$

(2) two-term virial equation:

$$V = \frac{RT}{P} + B = 3934 - 388 = 3546 \text{ cm}^3/\text{mol} \longrightarrow Z = \frac{PV}{RT} = 0.9014$$

(3) three-term virial equation:

$$V_{i+1} = \frac{RT}{P} \left(1 + \frac{B}{V_i} + \frac{C}{V_i^2} \right) = 3934 \left(1 + \frac{-388}{3934} + \frac{-26000}{(3934)^2} \right) = 3539 \text{ cm}^3/\text{mol} \quad 1^{\text{st}} \text{ iteration}$$

Ideal gas value

...

After 5 iterations

$$V_4 \sim V_5 = 3488 \text{ cm}^3/\text{mol} \longrightarrow Z = \frac{PV}{RT} = 0.8866$$

Generalized correlations for gases (Korelasi Umum)

- Pitzer correlations for the compressibility factor:

- $Z^0 = F^0(T_r, P_r)$

$$Z = Z^0 + \omega Z^1$$

- Simple linear relation between Z and ω for given values of T_r and P_r .
 - Of the Pitzer-type correlations available, the Lee/Kesler correlation provides reliable results for gases which are nonpolar or only slightly polar (App. E, table E.1 – E.4)).
 - Only tabular nature (disadvantage)

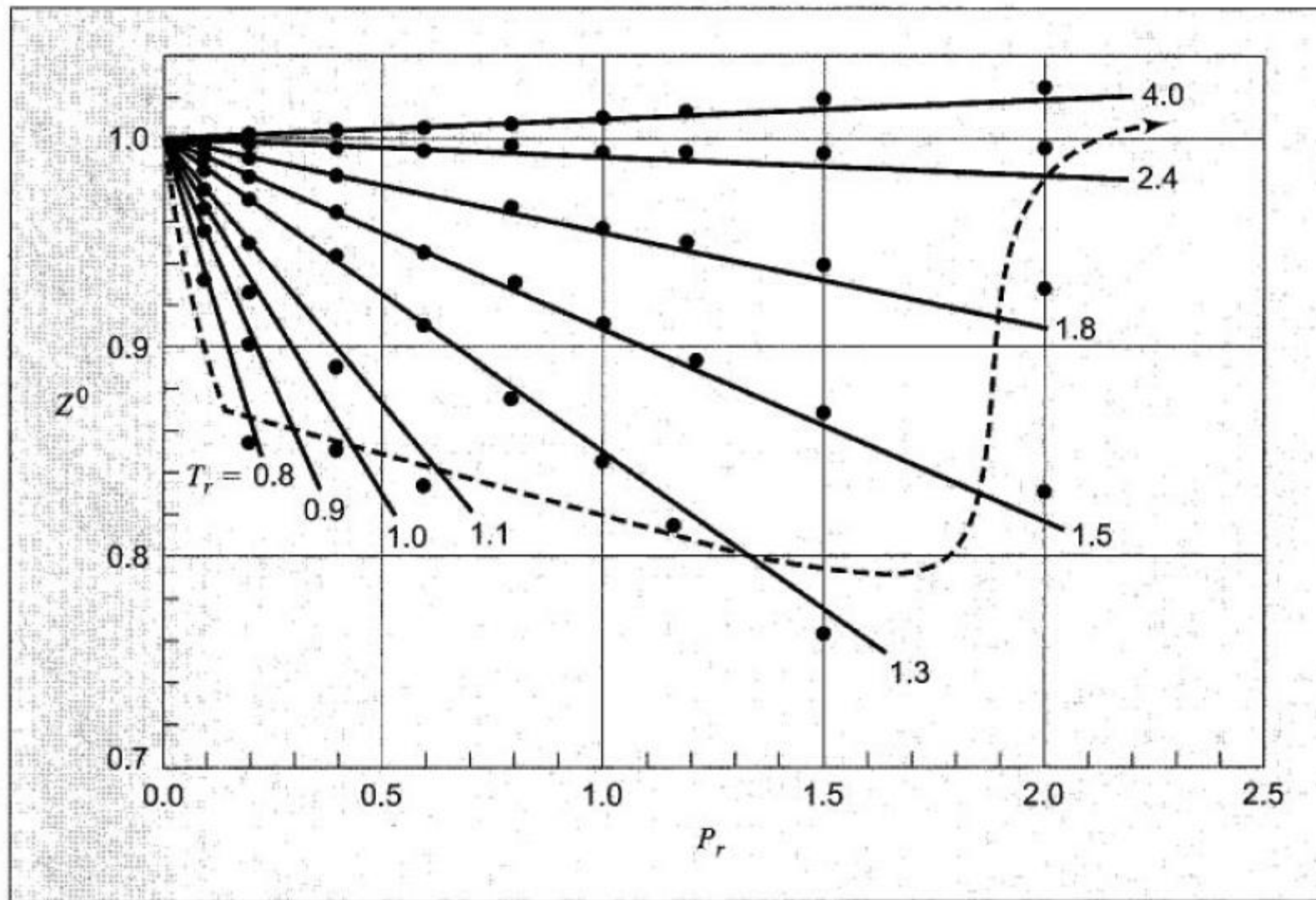


Figure 3.15 Comparison of correlations for Z^0 . The virial-coefficient correlation is represented by the straight lines; the Lee/Kesler correlation, by the points. In the region above the dashed line the two correlations differ by less than 2%

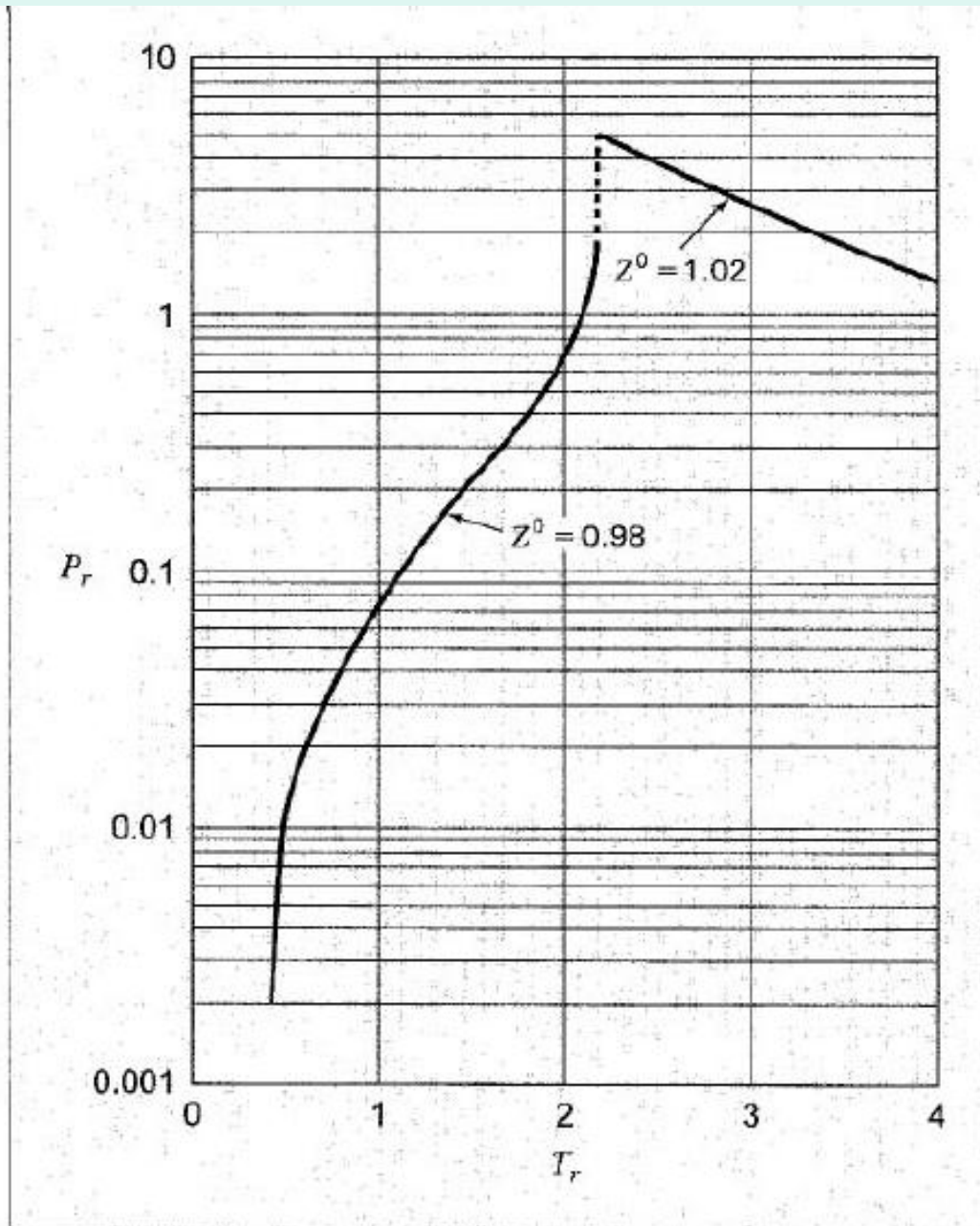


Figure 3.16 Region where Z^0 lies between 0.98 and 1.02, and the ideal-gas equation is a reasonable approximation

- Selain tersedia dalam bentuk tabel, metode Lee Kesler juga menyediakan bentuk grafik

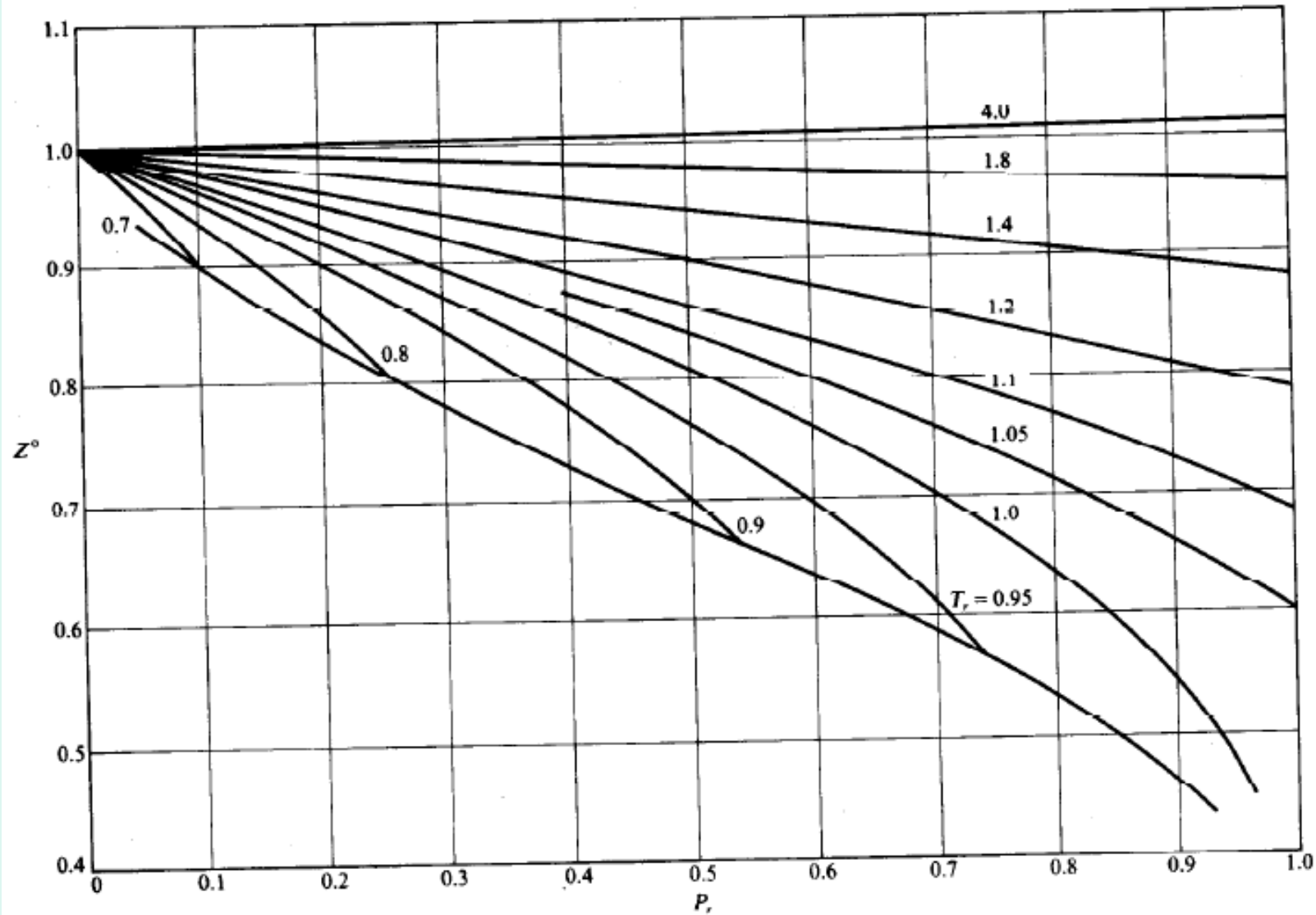


Figure 3.12 Generalized correlation for Z^0 , $P_r < 1.0$. (Based on data of B. I. Lee and M. G. Kesler, *AIChE J.*, 21: 510-527, 1975.)

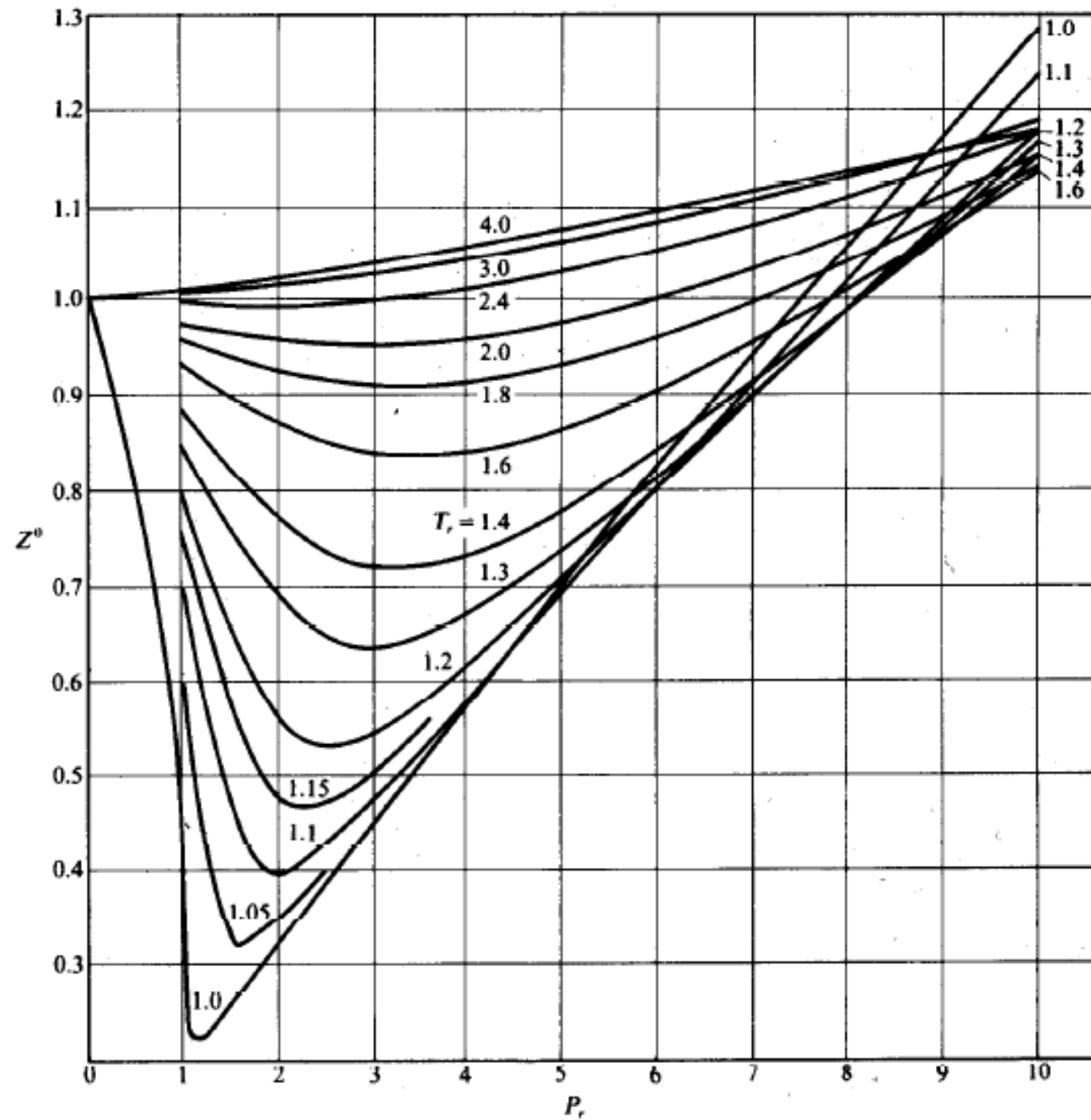


Figure 3.13 Generalized correlation for Z^0 , $P_r > 1.0$. (Based on data of B. I. Lee and M. G. Kesler, *ibid.*)

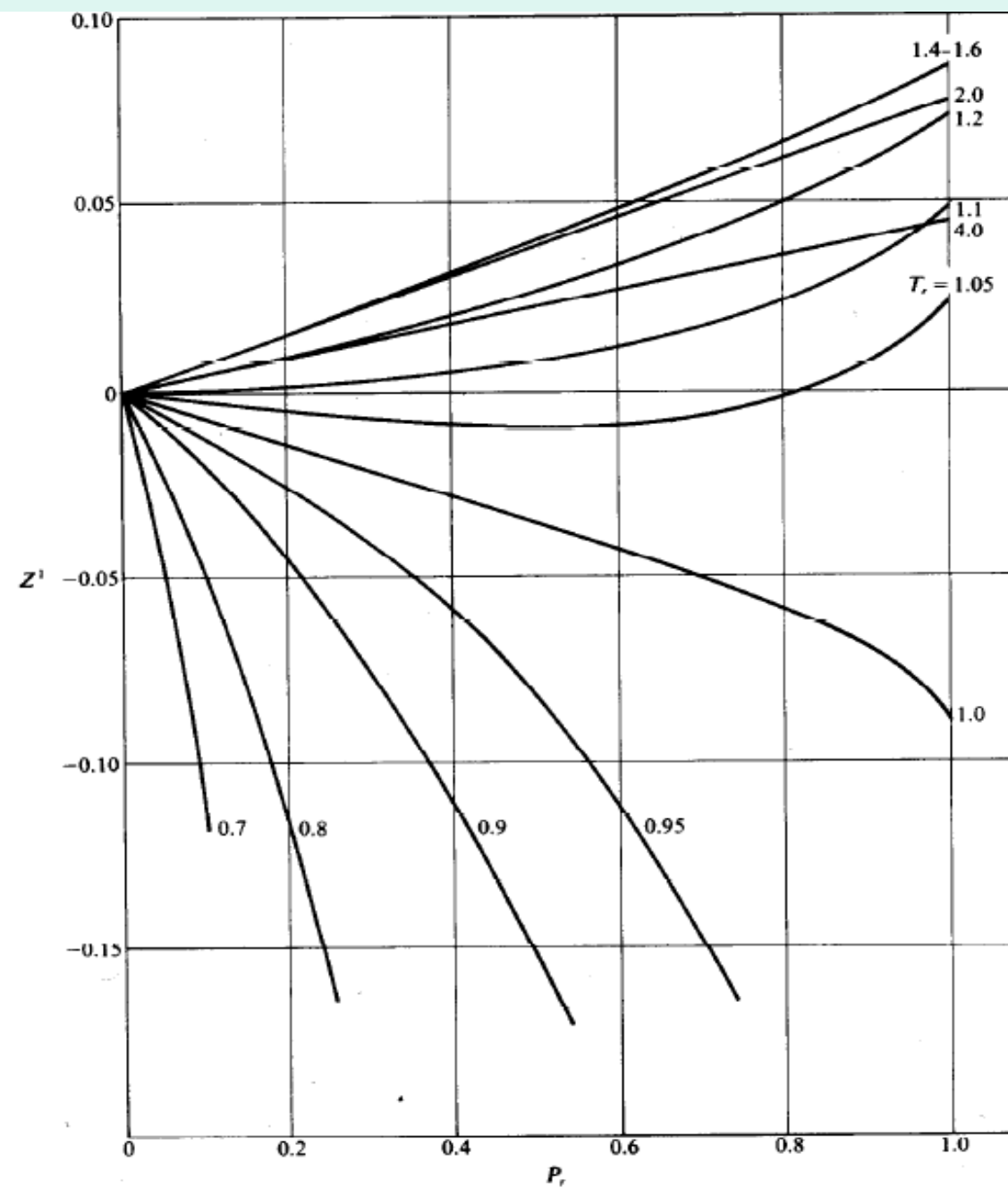


Figure 3.14 Generalized correlation for Z^1 , $P_r < 1.0$. (Based on data of B. I. Lee and M. G. Kesler, *ibid.*)

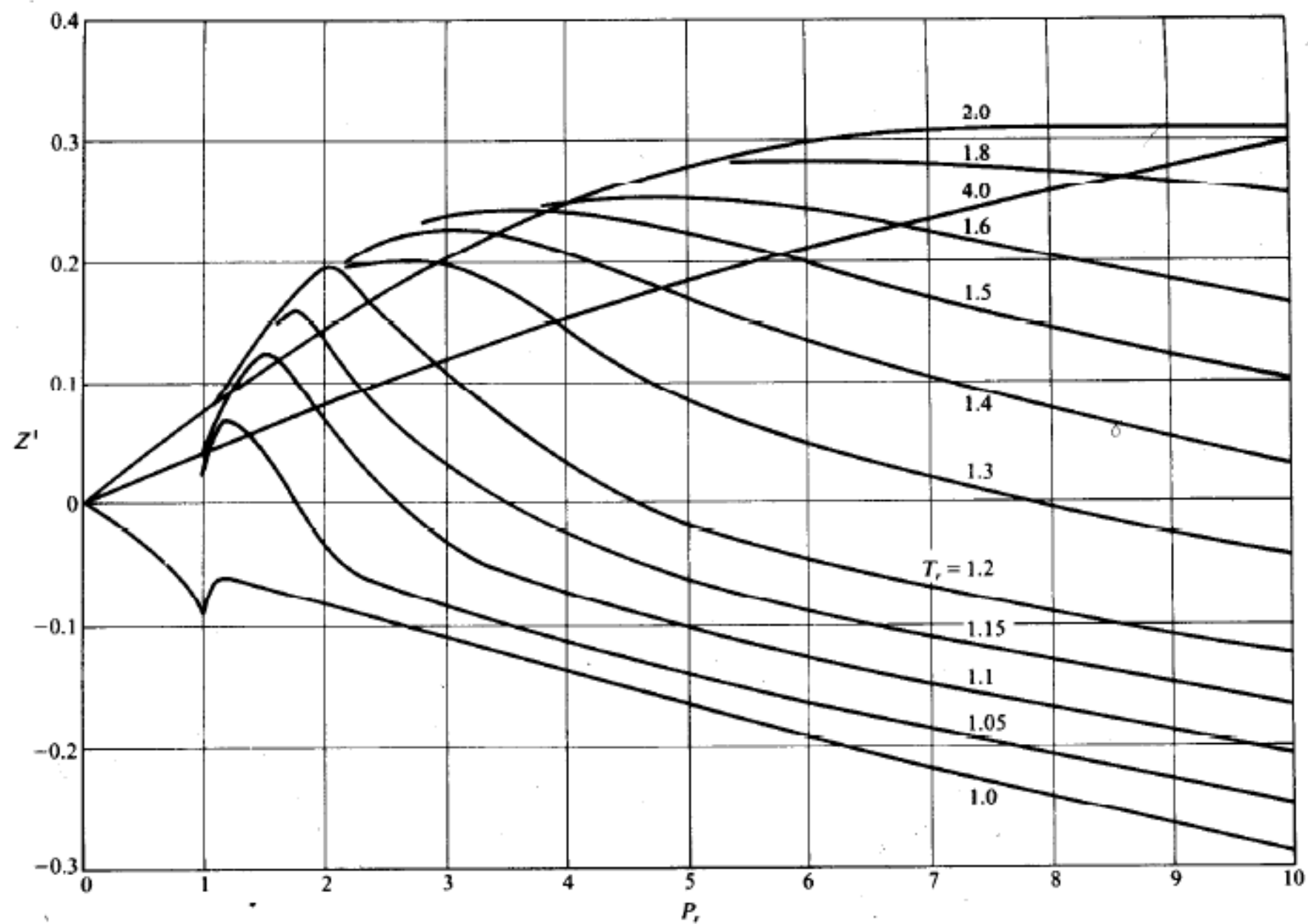


Figure 3.15 Generalized correlation for Z' , $P_r > 1.0$. (Based on data of B. I. Lee and M. G. Kesler, *ibid.*)

Pitzer correlations for the 2nd virial coefficient

- Correlation:

$$Z = 1 + \frac{BP}{RT} = 1 + B^0 \frac{P_r}{T_r} + \omega B^1 \frac{P_r}{T_r} \longleftrightarrow Z = Z^0 + \omega Z^1$$

$$Z^0 = 1 + B^0 \frac{P_r}{T_r} \quad Z^1 = B^1 \frac{P_r}{T_r}$$

- Validity at low to moderate pressures
- For reduced temperatures greater than $T_r \sim 3$, there appears to be no limitation on the pressure.
- Simple and recommended.
- Most accurate for nonpolar species.

$$B^0 = 0.083 - \frac{0.422}{T_r^{1.6}}$$

$$B^1 = 0.139 - \frac{0.172}{T_r^{4.2}}$$

Determine the molar volume of n-butane at 510K and 25 bar by, (1) the ideal-gas equation; (2) the generalized compressibility-factor correlation; (3) the generalized virial-coefficient correlation.

(1) The ideal-gas equation

$$V = \frac{RT}{P} = 1696.1 \frac{\text{cm}^3}{\text{mol}}$$

(2) The generalized compressibility-factor correlation

$$T_r = \frac{510}{425.1} = 1.200 \quad P_r = \frac{25}{37.96} = 0.659 \quad \xrightarrow{\text{the acentric factor}} \quad \omega = 0.200$$

the Lee/Kesler correlation

$$Z^0 = 0.865 \quad Z^1 = 0.038 \quad \rightarrow \quad Z = Z^0 + \omega Z^1 = 0.873 \quad V = \frac{ZRT}{P} = 1480.7 \frac{\text{cm}^3}{\text{mol}}$$

(3) The generalized virial-coefficient correlation

$$T_r = \frac{510}{425.1} = 1.200 \quad \left[B^0 = 0.083 - \frac{0.422}{T_r^{1.6}} \right] \quad \left[B^1 = 0.139 - \frac{0.172}{T_r^{4.2}} \right]$$

$$Z = 1 + B^0 \frac{P_r}{T_r} + \omega B^1 \frac{P_r}{T_r} = 0.879 \quad V = \frac{ZRT}{P} = 1489.1 \frac{\text{cm}^3}{\text{mol}}$$

What pressure is generated when 1 (lb mol) of methane is stored in a volume of 2 (ft)³ at 122°F using (1) the ideal-gas equation; (2) the Redlich/Kwong equation; (3) a generalized correlation .

(1) The ideal-gas equation

$$P = \frac{RT}{V} = \frac{0.7302(122 + 459.67)}{2} = 212.4 \text{ atm}$$

(2) The RK equation

$$T_r = \frac{581.67}{343.1} = 1.695 \quad a(T) = \Psi \frac{\alpha(T_r)R^2T_c^2}{P_c} = 453.94 \frac{\text{atm}}{\text{ft}^6} \quad b = \Omega \frac{RT_c}{P_c} = 0.4781 \text{ ft}^3$$

$$P = \frac{RT}{V - b} - \frac{a(T)}{V(V + b)} = 187.49 \text{ atm}$$

(3) The generalized compressibility-factor correlation is chosen (high pressure)

$$P = \frac{ZRT}{V} = \frac{Z(0.7302)(122 + 459.67)}{2} = 212.4Z \text{ atm}$$

$$P_r = \frac{P}{45.4} = \frac{Z}{0.2138} \quad T_r = \frac{581.67}{343.1} = 1.695$$

→ Z starts at Z = 1 and converges on Z = 0.890

$$P = 189.0 \text{ atm}$$

A mass of 500 g of gases ammonia is contained in a 30000 cm³ vessel immersed in a constant-temperature bath at 65°C. Calculate the pressure of the gas by (1) the ideal-gas equation; (2) a generalized correlation .

$$V = \frac{V^t}{n} = 1021.2 \frac{\text{cm}^3}{\text{mol}}$$

(1) The ideal-gas equation

$$P = \frac{RT}{V} = 27.53 \text{ bar}$$

(2) The generalized virial-coefficient correlation is chosen (low pressure, $P_r \sim 3$)

$$T_r = \frac{338.15}{405.7} = 0.834$$

$$P_r \sim \frac{27.53}{112.8} = 0.244$$

$$B^0 = 0.083 - \frac{0.422}{T_r^{1.6}}$$

$$B^1 = 0.139 - \frac{0.172}{T_r^{4.2}}$$

the acentric factor $\omega = 0.253$

$$Z = 1 + (B^0 + \omega B^1) \frac{P_r}{T_r} = 1 - 0.541 \frac{P_r}{T_r}$$

$$P = \frac{ZRT}{V} = 23.76 \text{ bar}$$

Generalized correlations for liquids

- The generalized cubic equation of state (low accuracy)
- The Lee/Kesler correlation includes data for subcooled liquids
 - Suitable for nonpolar and slightly polar fluids
- Estimation of molar volumes of saturated liquids
 - Rackett, 1970:
- Generalized density correlation for liquid (Lydersen, Greenkorn, and Hougen, 1955):

$$V^{sat} = V_c Z_c^{(1-T_r)^{0.2857}}$$

$$\rho_r \equiv \frac{\rho}{\rho_c} = \frac{V_c}{V}$$

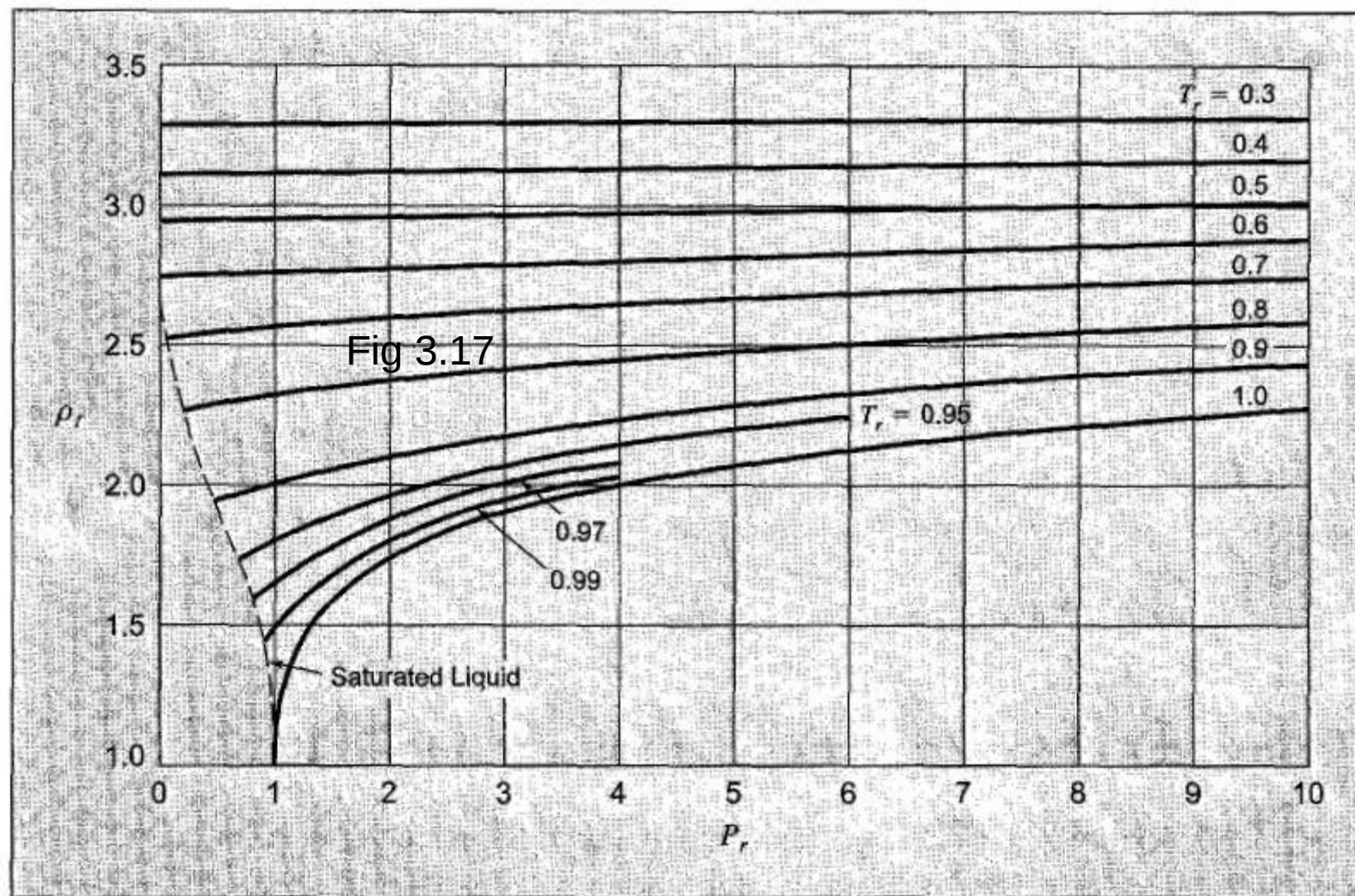


Figure 3.17 Generalized density correlation for liquids

$$V_2 = V_1 \frac{\rho_{r1}}{\rho_{r2}}$$

For ammonia at 310 K, estimate the density of (1) the saturated liquid; (2) the liquid at 100 bar

(1) Apply the Rackett equation at the reduced temperature

$$T_r = \frac{310}{405.7} = 0.7641 \quad V_c = 72.47 \quad Z_c = 0.242$$

$$V^{sat} = V_c Z_c^{(1-T_r)^{0.2857}} = 28.33 \frac{cm^3}{mol}$$

(2) At 100 bar

$$P_r = \frac{100}{112.8} = 0.887$$
$$T_r = \frac{310}{405.7} = 0.7641$$

Fig 3.17 →

$$\rho_r = 2.38$$

$$V = \frac{V_c}{\rho_r} = 30.45 \frac{cm^3}{mol}$$

$$V_2 = V_1 \frac{\rho_{r1}}{\rho_{r2}} = V^{310 K} \frac{\rho_{r1, 310 K, saturated liquid}}{\rho_{r2, 100 bar}} = 29.14 \frac{2.34}{2.38} = 28.65 \frac{cm^3}{mol}$$

Terimakasih